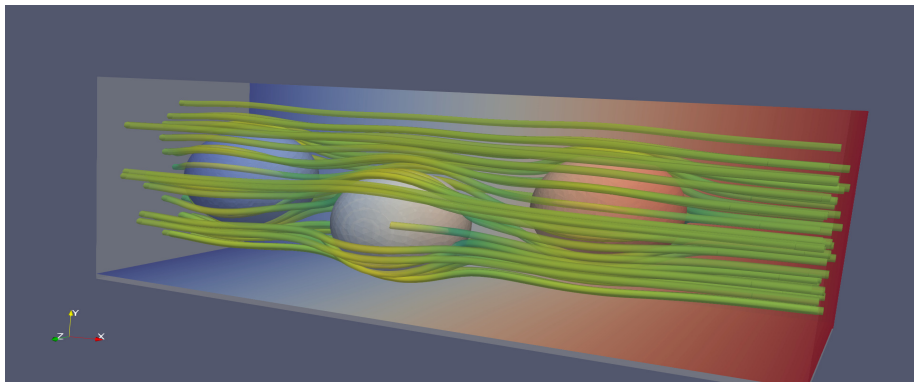




Limits of ion-trajectory control using electric field

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- normal sized satellites
(communication satellites,
astrophysical sat., ...) above 1000
kg
- small sized satellites
 - minisatellites : 500-1000 kg
 - microsatellites : < 500 kg
 - nanosatellites : < 50 kg
- CubeSats
 - multiple cubic modules
 - 10 cm per side
 - mass of 1.33 kg per unit
 - uses commercial off-the-shelf
components



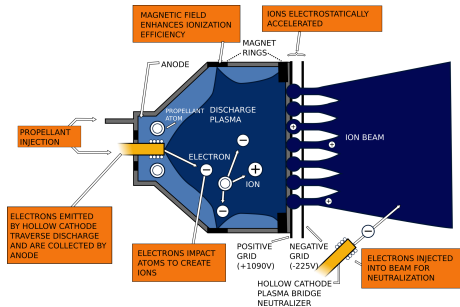
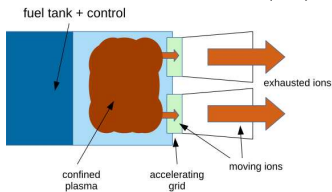


► components and methods that are commonly used in larger satellites are disallowed or limited (risk of explosion and weight restrictions)

- cold gas thrusters
 - inert gas stored and released through a nozzle to produce thrust
 - safe, but has low performance, attitude control usage
- chemical propulsion
 - a chemical reaction is used to produce a high-pressure, high-temperature gas that accelerates out of a nozzle
 - low complexity/high-thrust, but uses hazardous chemicals
- electric propulsion
 - electric energy used to accelerate propellant to high speed
 - only needs power, requires more solar panels, more complicated power distribution and larger batteries
- solar sail
 - using radiation sail (or solar pressure) to push ultrathin mirrors
 - no propellant required

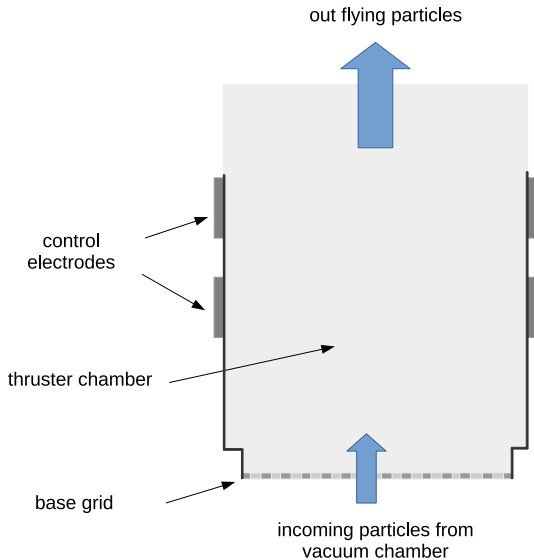


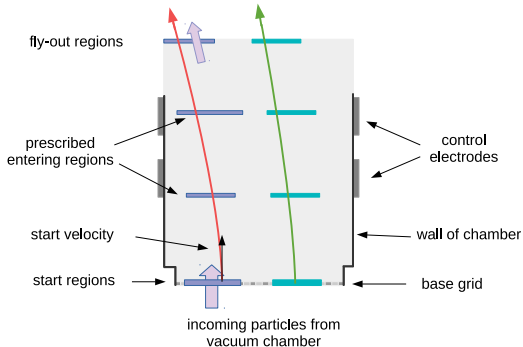
- creates thrust by accelerating ions using electricity
- neutral gas is ionized to create positive ions, that are accelerated by Coulomb-force along an electric field
- operation power : 1-7 kW (100 kW)
- exhaust terminal velocity : 20-50 km/s
- thrusts : 25-250 mN (5N)



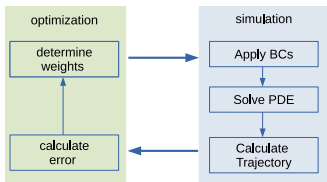


- accelerated ions fly through nozzle
- directing ion-jets (a small amount of ions) means ability of steering
- electrodes on the surface of nozzles generates electric field
- electric field deviates ions through Coulomb-force from straight flying





- accelerated ions fly through nozzle
- directing ion-jets means ability of steering
- prescribed path of ions are used for steering
- optimization algorithm determines electrode voltages





- particle trajectory : path of ion that travels through nozzle
- particle's equation of motion :

$$m_{ion} \cdot \frac{d^2 \vec{r}}{dt^2} = \vec{F}$$

- acting force calculated using electric potential
- electric potential is calculated using FEM (Finite Element) solver

equation to solve for

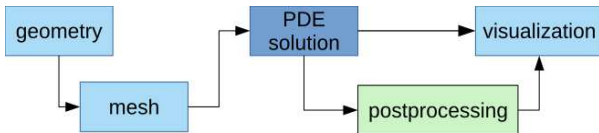
$$\nabla(\epsilon \nabla \phi) = 0$$

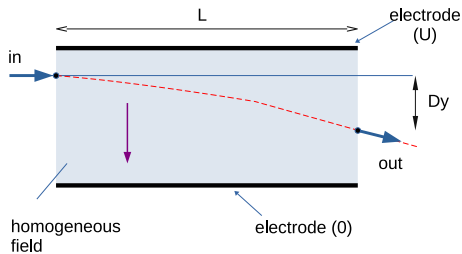
on surface of electrodes :

$$\phi_i = U_i$$

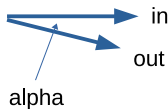
on other boundaries :

$$\left. \frac{\partial \phi}{\partial n} \right|_j = 0$$





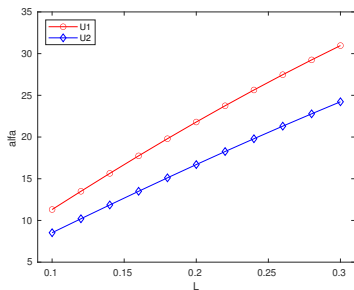
- ▶ simple model to estimate maximum deviation



- ▶ angle between velocity of out-flying and in-flying ions

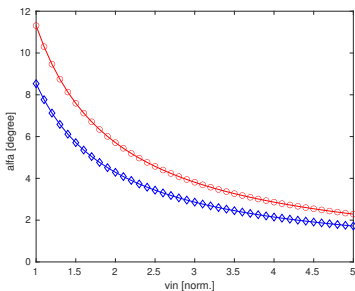
- plane capacitor (distance - D), maximum potential difference (U), length of capacitor (L)
- homogeneous field inside capacitor (purple arrow)
- angle of deviation (out - in) : α

$$\alpha \sim \arctan \left(K_0 \cdot U \cdot L \cdot v_{in}^2 \right)$$
- thrust force of deviation $\sim v_{in}^2$



► deviation angle ($^{\circ}$) as function electrode length (applied voltages : $U_1 > U_2$)

► longer electrode (along nozzle) means higher steering angle

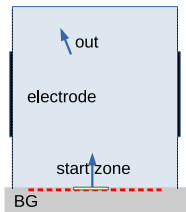


► deviation angle as a function ion's velocity (normalized) at start

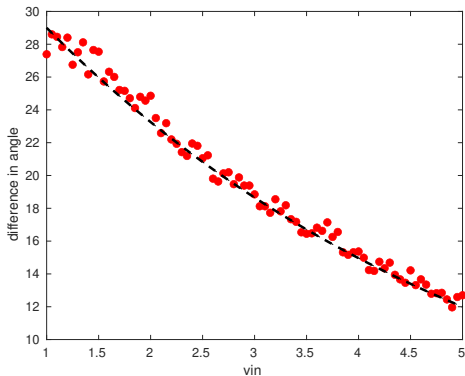
► higher velocity (smaller



- Simulated results of maximum deviation differs from results of simple model by 10-30 percent
- ions started from middle section of base grid
- difference of predicted and measured caused by inhomogeneous field of real electrode-system



- Difference of calculated and measured steering angle in percent





Conclusions

- electrodes' potential causes deviation of flying trajectory of ions (steering angle)
- steering angle is **small** at *high* ion velocity but **relatively high** thrust force
- *low* ion velocity means **higher** steering angle with **lower** thrust force
- optimization algorithm can take account of predicted maximum steering angles for different sections of starting zone

What to do?

- 3D extension of estimation model
- generating a steering angle map for optimization algorithm