

Limits of pathline control using electric field

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Abstract—Nowadays, CubeSat-sized satellites have become popular. A possible propulsion system for these satellites can be based on an ion thruster. In an earlier paper, we presented a possible way of calculating control parameters based on a prescribed ion pathline. This paper presents the limits of realizable paths based on theoretical calculations and 3D simulations.

Index Terms—electrostatic model, ion thruster, optimization, limitations

I. INTRODUCTION

In the recent years a lot of small satellites were launched that were designed and manufactured at our department (MaSat-1, SMOG-P [1], ATL-1[2], HRC-100) 1. In the next decade there will be the dawn of tiny sized satellites due to its relatively low cost of fabrication and space launch. There is a theoretical elkepzeles that control of satellites in orbit can be achieved using a small sized ion thruster (concept of ionthruster shown on Fig. 2).

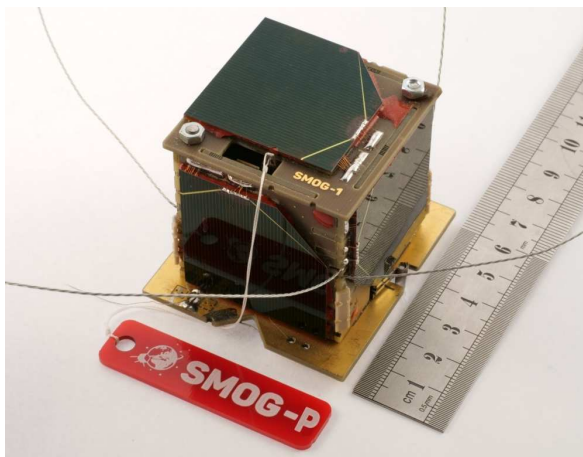


Fig. 1. Pocketcube (5cm×5cm×5cm sized) satellite [1]

II. ION PROPULSION SYSTEM OF SMALL SATELLITES

Az ionhajtóművek az elektromos meghajto rendszerek egy fajtája. Működésük alapját Newton 3. törvénye adja. A hajtóerőt ionok gyorsításával és kifelé történő lövésével érjük el. Az ionok haladásából keletkező impulzussal ellentétesen irányban lokodik a satellit. A rendszer fő részeit bemutató ábra látható see Fig. 2.

A vákuum kamra (1), amelyben elektromos tér segítségével a beáramoltatott xenon-ból ionokat hozunk létre (2) - confined plasma). Ennek egy részét a plazma fenntartásáért használjuk el. Egy másik részét a gyorsító rácokra kapcsolt elektromos feszültség keltette (közeli)

Krisztián Vida is at that time a graduating student of the department.

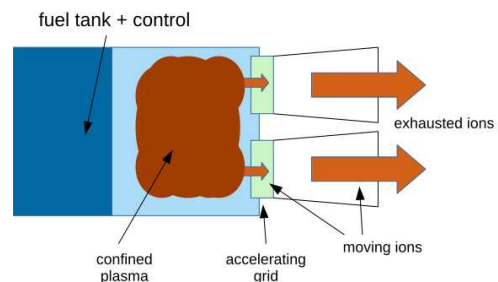


Fig. 2. Outline of an ion thruster system

egyenletes elektromos tér segítségével felgyorsítjuk és egy fúvókán keresztül a külvilág felé lövük. Az AG felső részén helyezkedik el egy fúvóka, amelynek felületén elektrodák helyezkednek. Az elektrodák potenciálja változtatható relative to the top of acceleration grid.

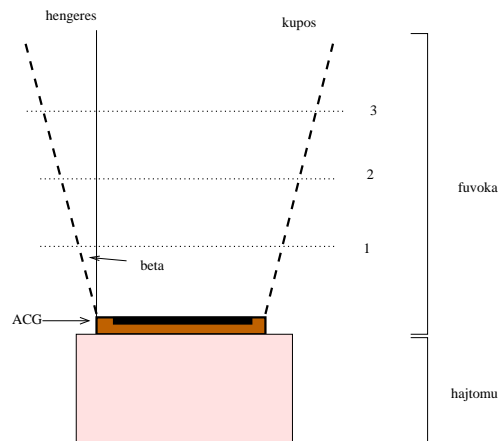


Fig. 3. Schematic of the nozzle with control electrodes on the surface

Az elkepzelesek szerint a 3 alapon a fúvóka felületén lévő elektrodák feszültségével létrehozott nem egyenletes elektromos hatására az elektromosan töltött ionok mozgásiránya megváltozik. On Fig. reffig:out1. láthatóan a fúvókán több layerben helyezkednek el a vezérlő elektrodák. A felgyorsított ionok hatására létrejövő toltóerő irányát az ionnyaláb kilepési irányának megváltoztatásával lehet befolyásolni.

In an earlier work [6] we showed the possibility of

optimization of ion trajectories (ion paths) in two-dimensional cases. In this paper we analyze the maximum of the achievable declination angle in case of 2- and 3-dimensional nozzle designs.

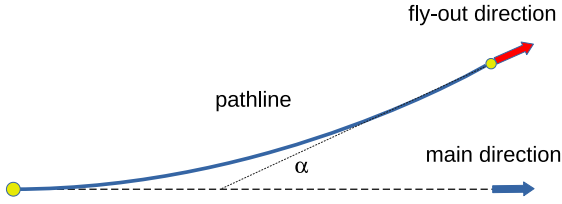


Fig. 4. Definition of declination angle (α) as tilt angle of two lines (line of main direction and line of fly-out direction). Ion starts from the left and travels through pathline.

III. PHYSICAL MODEL OF PROBLEM

We used a simple electrostatic model of the nozzle that consists of control electrodes and a plate at a given electrostatic potential as boundary conditions [3]. Usage of electrostatic approximation is acceptable due to low potential change rates and relatively high ion speed.

$$\nabla(\varepsilon \nabla \varphi) = 0 \quad (1)$$

Using calculated potential we can determine the pathline of ions starting from the top of acceleration grid, solving the following equation [4]

$$m \cdot \frac{d^2 \vec{r}_{ion}}{dt^2} = \vec{E} = -\nabla \varphi + \vec{E}_{ext} \quad (2)$$

where \vec{r}_{ion} is location of ion and \vec{E}_{ext} models non-electric forces.

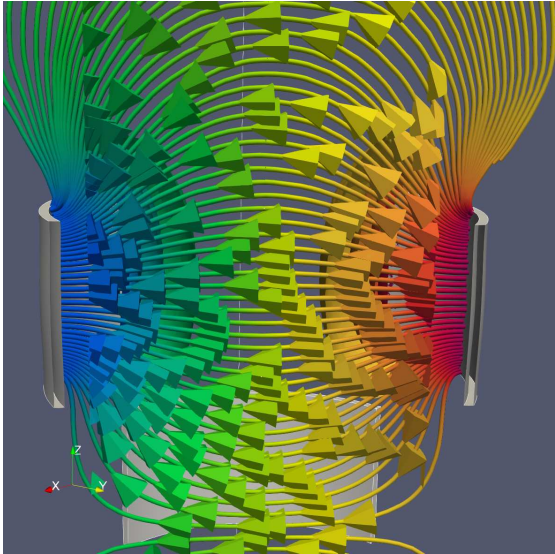


Fig. 5. Electric field lines shown between two electrodes. Color indicates electric potential of the point. Notable the nearly homogeneous field in the middle region and higher nonhomogeneity on the outer region.

IV. APPROXIMATIVE MODEL IN ONE DIMENSION

In this case we are focused on the two-dimensional case of nozzles. It is a good approximation if control electrodes are

We use the simplest feasible model. Electrodes form a plane capacitor (infinite plane electrodes with constant distance, d) with length L and electric potential difference U as shown on Fig. 6. The declination angle can be calculated as function of potential difference, ion speed and electrode length [3].

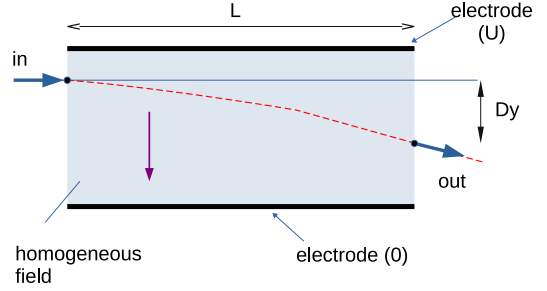


Fig. 6. Simple (plane capacitor) model to calculate an approximation of declination angle

By choosing potential of the electrodes properly, different types of control patterns can be realized. Usage of symmetrical potentials results simple bending of pathlines, that can be characterized using a bending angle (α) [6].

In case of more complex potential arrangement more complex pathlines can be achieved. We examine these more complex effects using a 3D model. We present a 2D/3D FEM model solution with optimization.

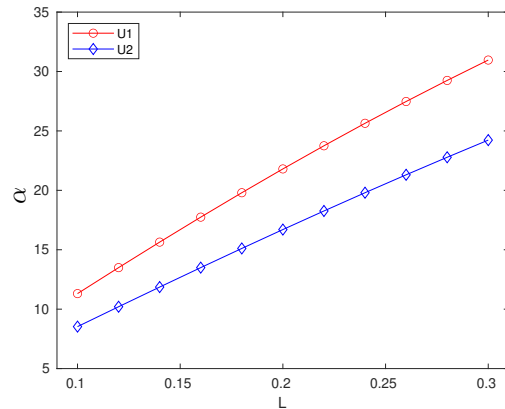


Fig. 7. Declination angle(α) as a function of electrode length(L) in case of different electrode potential difference.

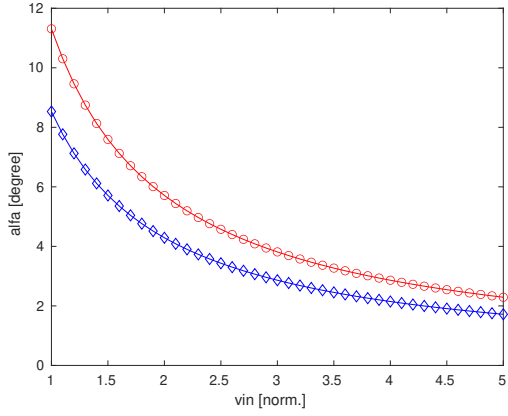


Fig. 8. Declination angle(α) as a function of starting speed of electrons entering electrode(v_{in}).

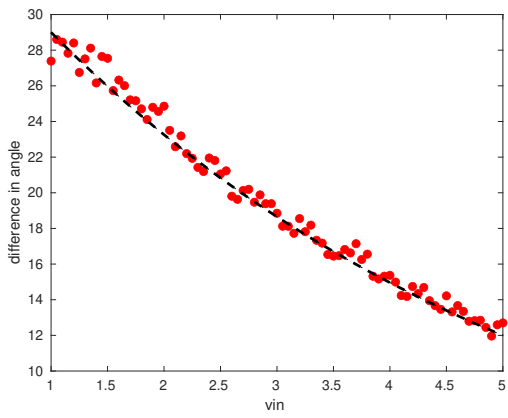


Fig. 9. Declination angle(α) as a function of starting speed of electrons entering electrode(v_{in}).

V. THREE DIMENSIONAL EFFECTS

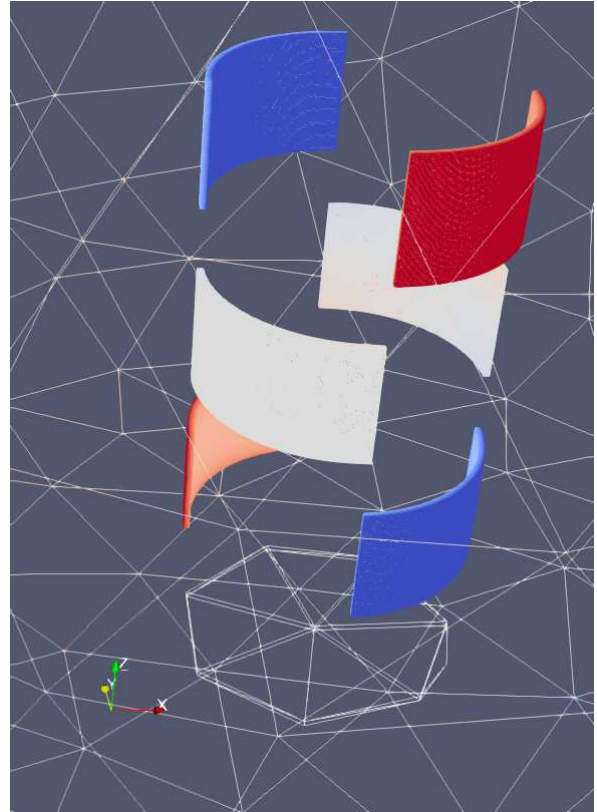


Fig. 10. Electrodes that control ion pathlines. Red electrodes are set to "high" voltage, blue electrodes are set to "low" voltage, grey electrodes are not connected.

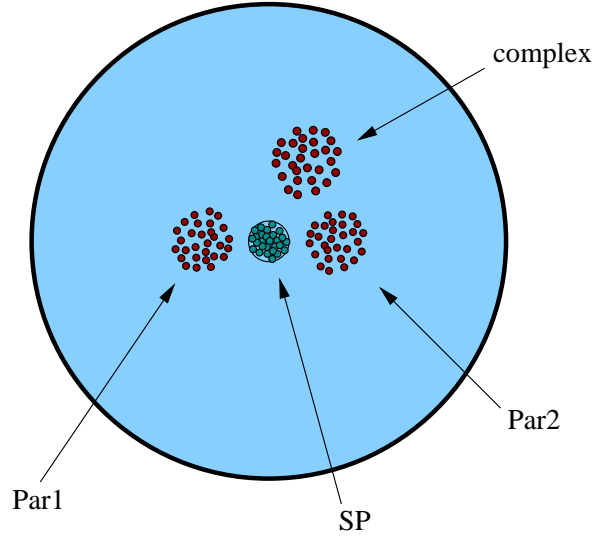


Fig. 11.

VI. CONCLUSIONS

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